Relation between various chromium compounds and some other elements in fumes from manual metal arc stainless steel welding

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Abstract

For the years 1987-1990 160 individual samples of manual metal arc stainless steel (MMA/SS) welding fumes from the breathing zone of welders in four industrial plants were collected. Concentrations of soluble and insoluble chromium (Cr) III and Cr VI compounds as well as of some other welding fume elements (Fe, Mn, Ni, F) were determined. Concentration of welding fumes in the breathing zone ranged from 0.2 to 23.4 mg/m3. Total Cr amounted to 0.005-0.991 mg/m3 (including 0.005-0.842 mg/m3 Cr VI). Total Cr content of fumes varied from 0.1 to 7.4%. The distribution of particular Cr compounds was: 52.6% soluble Cr (including 50.7% Cr VI), 65.5% total Cr VI, and 11.4% insoluble Cr VI. The results obtained indicate that MMA/SS welding is a process that could be highly hazardous to human health. Evaluation of occupational exposure has shown that MMA/SS welders may exceed the admissible concentrations of soluble and insoluble Cr VI forms as well as of Mn and Ni. In the plants investigated the sum of the ratios of concentrations of particular welding fumes in the breathing zone of welders exceeded corresponding maximum allowable concentration values by 24 times (including 17 times for total Cr VI). Due to the variety and changeability of particular parameters occurring in the working environment, the composition of MMA/SS welding fumes (in the welder's breathing zone) is so variable that it is not possible to assess the exposure by means of

one universal exposure indicator (maximum additive hygienic limit value). The evaluation should be based on the results of measurements of concentrations of particular elements in welding fumes.

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Occupational exposure to chromium (Cr) poses a serious problem and many studies on the biological effects of chromates have been conducted. Chromates are well recognised as human carcinogens and suspected of genotoxic action.: 45

Numerous epidemiological studies have been carried out to determine the relation between human exposure to chromates and the occurrence of lung cancer, but only some of them include measurements of exposure in stainless steel (SS) welders." The level of exposure of workers to metal fumes, fluxes, and gases depends, to a large extent, on the type of welding. Welding techniques vary, although most stainless steel welding is performed with electric arc (manual metal arc (MMA)) processes.

The chemical composition of MMA/SS welding fumes and details of occupational exposure of welders in the workplace have been reviewed. Particular attention has been paid to Croxidation state in welding fumes.' 9

A few studies devoted to occupational exposure of MMAiSS welders have considered Cr compounds of different solubilities and at different oxidation states.' ¹⁰ In our previous studies, the analytical procedure for simultaneous determination of soluble and insoluble Cr III and Cr VI as well as of some other elements in welding fumes was presented for evaluation of occupational exposure of welders. ¹¹⁻¹⁵

This study was aimed at evaluation of welders' occupational exposure to Cr III and Cr VI compounds, as well as to some other elements in MMA/SS welding fumes, in selected Polish industries.

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Materials and methods SUBJECTS AND EXPOSURE

The study covered the workers at a plant where some

Table I Composition of welding materials

Plants	Stainless steel		Content		
		Electrode rype	Cr /%)	Ni '°o	
A	1H18 N9T	ES 18-8 SiBB ES 18-8 2B	18	8	
В	08H18 N1OF	EA 400/10T EA 395/9 AVESTA P-5	17-19 13 5-17 22	9–12 22–25 12–14	
C	OH 17 T	ES 20-1-6B	18	8	
D	H 18 N9T	ES 188B MVRAC/DC(AR)	18 19 5	8 10	

items of equipment for power stations were manufactured (A), a chemical industry plant (B), and two metal industry plants (C, D). All plants were equipped with dilution ventilation with blowing and exhaust systems. Local exhaust systems were used only at the welding sites in plant C. Table 1 presents the materials used in the welding process in particular plants.

PROCEDURE

Throughour 1988-90 about 120 individual samples of MMA/SS welding fumes in the breathing zone of welders and 40 individual samples from welder assistants in the four industrial plants (A, B, C, D) were collected. During the regular eight hour shift the welders were occupied either with welding or with assembly work connected with the welding process for about six and a half to seven hours. Two air samples a shift were collected simultaneously in a welder's breathing zone (behind the face guard), each over a period of about seven hours. Two stage personal air sampling was applied (Casella AFC-123, flow rate 1.9 l/min). The respirable fraction of dust was collected on a membrane filter (Sartorius 11304, $0.8 \,\mu\text{m}$, Ø37 mm) and a glass fibre filter (Whatman GF/A, 037 mm). Methods of sample collection, preparation, and analytical procedures have been presented earlier." 12

Before and after sampling filters were dried at 105°C for one hour, then cooled in a desiccator and weighed. Next the mass of dry substance was calculated by comparing filter mass before and after the sampling.

Membranefilter

In one part of the sample from the membrane filter Fe, Mn, Ni, and Cr were determined by atomic absorption spectroscopy. In the other part of the membrane filter sample, fluorides were determined after microdiffusion using a colorimetric method with a zirconium-SPANDS complex.

Glass fibrefilter

In one part of the glass filter total soluble Cr was determined by atomic absorption spectroscopy after water extraction. Soluble Cr III was separated from soluble Cr VI in a column filled with s-diphenylcarbazide resin, which retains Cr VI. Soluble Cr III was determined in the eluate. After alkaline extraction of the sample, insoluble Cr VI was determined in the insoluble residue by a colorimetric method with s-

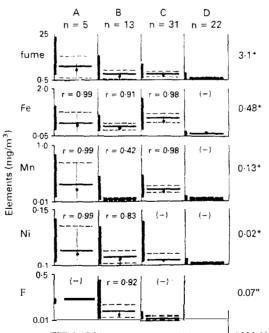


Figure 1 TWA (8 h) concentrations of elements in MMA! SS welding frames (m8/m³). TWA=time weighted average; A, B, C, D = plants; = range of concentrations; = arithmetic mean (with confidence intervals);

• = geometric mean (with conjdence intervals); * = mean values & concentrarrons in all tested plants; r = correlation coefficient; n = number of measuremenrs; (-) = no correlation (p > 0.05).

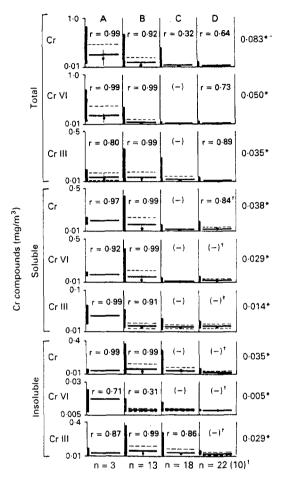


Figure 2 TWA (8 hi concentrations of particular Cr compounds in MMA|SS welding fumes (mg/m^3) (explanations as infig 1).

diphenylcarbazine. The second part of the glass filter was used to assess the content of total Cr VI by the same method. All other Cr values were calculated by difference.

Results

Figures 1 and 2 present the time weighted average concentrations (TWA-8h) of welding fumes and their major elements (Fe, Mn, Ni, F, Cr) as well as of particular Cr forms (soluble and insoluble Cr III and Cr VI) in the air (mg/m^3) of the particular industrial plants (A,B,C,D). They also show mean concentration values from all plants. Welding fume concentrations in the welders' breathing zone ranged from 0.2 to 23.4 mg/m³. The maximum concentration was found in plant A (mean 9.0 mg/m³; range $2\cdot8-23\cdot4$

mg/m³). In plant C, considerably higher concentrations of fumes were found in the welders' breathing zone (mean 3.5 mg/m^3 ; range $1.0-9.1 \text{ mg/m}^3$) than in that of the welders' assistants (mean 0.8mg/m^3 ; range $0.2-1.9 \text{ mg/m}^3$) who only occasionally stayed at the welding posts. Mean fume concentrations in plants B and D amounted to 3.2 mg/m^3 and 1.3 mg/m^3 respectively.

Similar values of respirable dust fraction concentrations were obtained in the samples collected in the breathing zone of welders simultaneously on a membrane filter and a glass fibre filter (r = 0.75-0.98).

Mean weighted total Cr concentration in the breathing zone of welders ranged from 0.005 to 0.991 mg/m³ (fig 2). The highest total Cr concentration was found in plants A and B in which the work was performed in a half closed area without local exhausts and in a forced body position.

Figure 3 presents the content of particular 'elements of fumes. The data indicate that the chemical content of fumes in the breathing zone of welders varied greatly. Total Cr in the fumes occurring in the breathing zone of all welders ranged from 0·1% to 7·4%. Mean values of total Cr (Yo) in plants A, B, C, and D were 3·4%, 2·5%, 1·4%, and 2·6% respectively.

The relations between concentrations of particular constituents—namely, Fe, Mn, Ni, and Cr—and concentration of fumes are presented in the form of correlation coefficients and regressions of the type y = a + bx in particular plants (fig 1) and graphically in the form of simplified lines of the typey $= kx \pm k$ for all plants (fig 4). A low correlation coefficient and lack of linear dependence were obtained for total Cr in plant C (welders and their assistants together; fig 2). Figure 4 presents graphically the relation between concentrations obtained for all plants (disregarding welders' assistants from plant C). Total Cr concentration with regard to fumes was characterised by a high correlation coefficient (r = 0.89).

The results obtained from regression lines (n = 59, p = 0.05) have facilitated calculation of the mean content of particular elements in fumes (table 2).

Similar relations were determined for concentrations of particular Cr forms with regard to fume concentration in all plants tested. Figure 5 presents these graphically. Table 3 shows the mean content (%) of particular Cr forms in the fumes. This was determined from regression lines $y = kx \pm k$. Participation of particular Cr forms in relation to total Cr was determined in the same way (fig 6, table 4). The relations presented indicate that participation of particular Cr forms compared with total Cr content in all samples determined (samples exceeding the sensitivity of the method) was similar (table 4).

Due to considerable variability in the content of fumes in the MMA/SS welders' breathing zone, the evaluation of exposure was based on TWA (8 h)

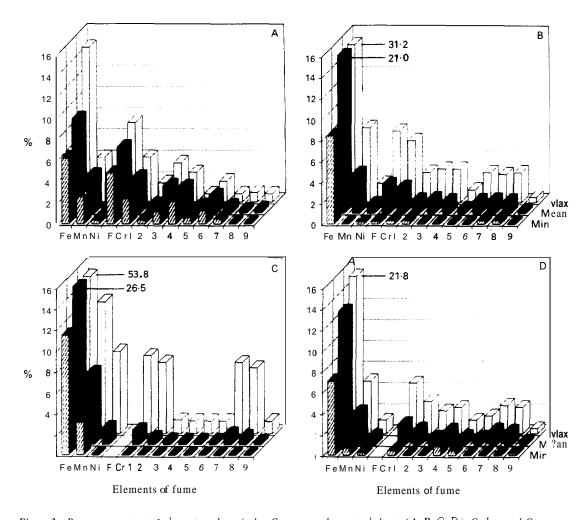


Figure 3 Percentage content of elements and particular Cr compounds in tested plants (A,B,C,D). Cr 1 = rotal Cr; 2 = soluble Cr; 3 = soluble Cr III; 4 = soluble Cr VI; 5 = total Cr VI; 6 = insoluble Cr; 7 = insoluble Cr III; 8 = insoluble CrVI; 9 = roral Cr III.

concentrations of fumes for particular elements (Fe, Mn, Ni, F, Cr VI, Cr 111) adopting the principle of their cumulative toxic effect. The evaluation of combined occupational exposure (figs 7-9) allowed us to ascertain that maximum allowable concentrations (MAC) values were exceeded in 42.5% of MMA/SS welders (n=72). Individual welders' combined exposure to the elements in fumes was 24 times the admissible value for Cr VI, 17 rimes for Ni and three times for Mn in plant A (fig 7). The hygienic standards for various Cr forms, mandatory in some other countries, were exceeded for total Cr VI and soluble Cr VI in 23-25% of results and for soluble Cr VI in 5% of results, whereas no form of Cr III exceeded hygienic standards (table 5).

Discussion

The concentration of MMAiSS welding fumes may vary in particular workplaces from a few to several hundred mg/m³.²⁸ Stern, "²¹ generalised the data for Swedish and Danish workplaces and found that for MMA/SS processes the medium TWA (8h) total dust concentration in the breathing zone varied from 1.5 to 10 mg/m³. An indicator of the range of exposures to total particles was provided by Ulfvarson.16

Our studies, performed in derail for the first time in Polish industry, indicated that the TWA (8h) of respirable fraction of MMA/SS fumes in the welders breathing zone ranged from 0.2 to 23.4 mg/m³ (mean 3.1 mg/m^3) (fig 1).

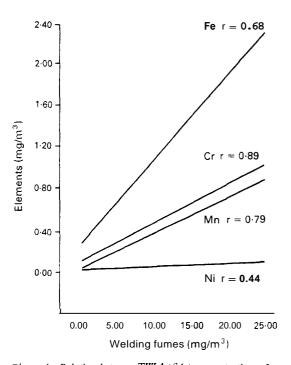


Figure 4 Relation between TWA(8h) concentrations of elements and MMAiSS welding fumes (plants A, B, C, D). Number of measurements performed; = 60. y = correlation line y=kx+ktor: Fe 0.112x+0.21; Mn0.039x+0.006; Ni0.005x+0.002; Cr0.036x+0.005.

The variations in concentration of particles depend on welding parameters and environmental factors. Working procedures and general and personal prevention systems have an influence on concentrations in fumes.

Also, the presence of some other processes applied in the vicinity affects the chemical composition of the background: under certain conditions, the background may significantly affect the fumes collected in the breathing zone, although usually the background concentration of fumes measured with stationary samplers constitutes about one tenth of that found in the breathing zone. 1617

Relations exist between concentrations of elements in fumes and distance from the welding area. The results of our studies indicate that MMA/SS fumes and their elements are usually more concentrated in

Table 2 Mean content σ the elements in MAA/SS welding fumes (plants A, B, C, D)

Elements (%)						
Fe	Mn	Cr	Ní	F		
11.2 (2.1	3-9 (0-6)	3.6 (0·5)	0.5 (02)	3 3 (0.6)		

Confidence intervals in parentheses.

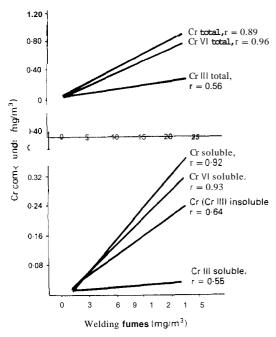


Figure 5 Relation between TWA (8 h) concentrations of parricular Cr cornpounds and MMA! SS welding fumes (plants A, B, C, D). y = correlation line $y = kx \pm k$ for: total Cr 0.036x ± 0.005 ; rotal Cr VI0.025x ± 0.003 ; total Cr III $0.011x \pm 0.003$; soluble Cr 0.023x ± 0.004 ; soluble Cr VI $0.023x \pm 0.004$; soluble Cr III $0.0123x \pm 0.004$; soluble Cr III $0.016x \pm 0.006$.

the breathing zone than in the workplaces.¹⁵ The individual samples may contain higher percentages of Cr and Mn compared with the stationary samples but a lower Fe percentage."¹⁷

The data published by the International Agency for Research on Cancer² show that evaluation of occupational exposure to fumes under some determined conditions can be estimated by combining information on the elemental abundance of the aerosol as determined from a chemical analysis of welding fumes produced in the laboratory under controlled conditions," and the total aerosol concentration expected on the basis of measurements in the workplace. The disadvantage of this technique, however, is that the actual composition of specific welding fumes cannot be determined.

Although the average percentage of elements in MMA/SS welding fumes found in our study (table 3) is similar to the percentage reported by some other authors (Cr 2-9·2; Ni 0·2-3·3; Fe 3·3-15·9; Mn 1·4-14%), 218-21 mean statistical values of particular elements in the welders' breathing zone do not form a real picture of exposure.

The data presented (fig 3) indicate that different conditions at the workplace may result in variations in the chemical composition of the fumes. Therefore,

Table 3 Mean content of particular Cr compounds in MMAISS welding fumes (plants A, B, C, D)

.r compounds (Cr)	No & measurements	% Crin fumes	N^\star	% Cr fume
Soluble Cr	44	1.7 (0.4)	28	2.3 (0.4)
Soluble Cr VI Fotal Cr VI	44 44	1.4 (0.4) 1·5 (0·4)	14	2.3 (0.5)
	60	2.5 (0.3)	35	2.9 (0·4)
nsoluble Cr III Fotal Cr III	44 44	1.3 (0.4) 1.6 (0.4)	28	1.6 (0.6)
	60	1.1 (0·3)	45	2.3 (0.5)

Confidence intervals in parentheses. "Number of measurements above detection limit

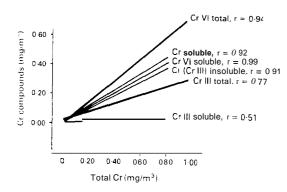


Figure 6 Relation between TWA (8h) concentrations of particular Cr compounds and toral Cr vin M M A SS welding fumes (plants A, B, C, D). v – correlation line y = $kx \pm k$ for: total Cr $VI0.685x \pm 0.076$; soluble Cr $0.526x \pm 0.073$; soluble Cr $0.526x \pm 0.073$; soluble Cr $0.526x \pm 0.073$; insoluble Cr $0.526x \pm 0.073$; soluble Cr $0.526x \pm 0.073$; $0.082x \pm 0.037$

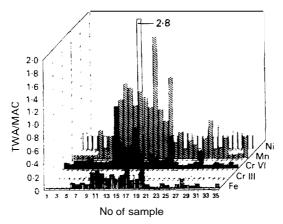


Figure 8 Occupational exposure to elements of MMA/SS welding fumes in plant C (explanation as in fig 7).

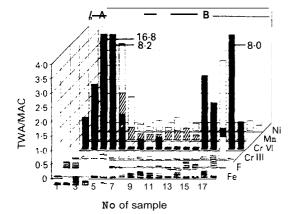


Figure 7 Occupational exposure to elements of MMA₁SS welding fumes in plants A, B TWA = time weighted average threshold limit values (Cr III 0.5 mg/m², Cr VI 0.05 mg/m²). MA C = maximum allowable concentration (Fe 5 mg/m³, M n 0.3 mg/m², Cr VI 0.05 mg/m²). (Ni 0.05 mg/m²)

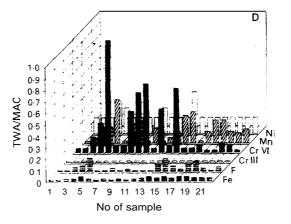


Figure 9 Occupational exposure to elements of MMA|SS weldingfumes in plant D (explanation as in fig 7).

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Table 4 Mean content of particular Cr compounds compared to total (plants A, B, C, D)

		Cr%		Cr % Total Cr	
Cr compounds (Cr)	No o t measuremenrs	Total Cr	N O *		
Soluble Cr	44	52.4 (5·7)	28	52.6 (7.3)	
Soluble Cr III	44	8.7 (2.7)	22	8.2 (3.7)	
Soluble Cr VI	44	44.7 (5.1)	14	50.7 (3.2)	
Total Cr VI	44	46.2 (5.0)			
	60	68.3 (5.7)	35	68.5 (7.6)	
Insoluble Cr	44	47.7 (5.5)	32	47.9 (6.6)	
Insoluble Cr III	44	45.6 (5.5)	28	46.0 (6.9)	
Total Cr III	44	53.9 (4.9)		` '	
	60	31.8 (5.8)	45	31.8 (6.7)	

Confidence intervals in parentheses. 'Number of measurements above detection limit.

Table 5 Occupational exposure of MMAISS welders to particular Cr compounds

	$No \geqslant TLV/No (max TWA TLV)$					
	Soluble		Toral	Insoluble		Toral
Plant	Cr III	Cr VI	Cr VI	Cr 111	Cr VI	Cr 111
A B C D A + B + C + D	= = = -	3/ 3 (3.7) 4/13 (15·4) 1/18 (1·3) 3/10 (2.0) 11/44 (15.4)	8/8 (16.8) 4/13 (8.0) 1/18 (1.0) 1/22 (1.0) 14/60 (16.8)	_ _ _ _	1/13 (1.3) 1/18 (1·3) 2/41 (1·3)	
TLV (mg/m³)	0.525	0 02526	0 0525	0.525	0.012627	0 5'5

TLV = threshold limit value; TWA = time weighted average.

individual measurements in the breathing zone of welders during a shift are absolutely necessary to determine the risk of exposure.

In recent studies' 9 considerable attention has been paid to the oxidation state of Cr in welding fumes, and it has always been taken into account in our previous¹⁵ and current studies. In most studies on MMA/SS fumes, the concentration of Cr VI (mostly water soluble) ranged from 0·025 to 1·550 mg/m³.2 9 10 22

In our studies, the occurrence of high concentrations of Cr VI in MMAiSS fumes (range 0·005–0·8 mg/m³; fig 2) was confirmed as well as a high relative content of total Cr VI with high concentrations of soluble Cr VI (tables 2–4, figs 3–6). A considerable excess over the hygienic standards for individual exposure^{25–29} was also noted (table 5, figs 7–9).

The high Cr VI content (36–100% of total Cr) in MMA/SS fumes in attributed to the presence of alkaline metals in the flux coating. In the study of Kobayashi and Tsutsumi, ²³ potassium was replaced by sodium in a modified electrode, resulting in a significant reduction in the relative Cr VI content (soluble Cr VI -5.6%, insoluble Cr VI -11.2%). Actually, the insoluble Cr VI content in MMA/SS

welding fumes ranged from 0.03 to $0.92\%^{2.18\,21.24}$ and CrO₃ content from 0.4–1.8%. The mean value of 0.2–0.3% is negligible from the point of view of exposure.'

In our study, however, we found that insoluble Cr VI content in welding fumes varied from 0.1 to 1.2%, in dust with an average 0.3%.

The data on the insoluble Cr VI content in MMA/SS welding fumes, especially in industry, have been a subject of discussion. Taking into account the fact that Cr VI has been considered to be a human carcinogen: no safe level for Cr VI can be recommended. It seems that its occurrence in fumes even at a concentration less than $0.005-0.842 \text{ mg/m}^3$ may create a serious health risk (fig 2, table 5).

CONCLUSIONS

Evaluation of occupational exposure has indicated that MMA/SS welders may exceed the admissible concentrations of soluble and insoluble Cr VI, Mn, and Ni.

Due to various changeable parameters in the working environment, the content of fumes in the welders' breathing zone is not constant and hence it is not possible to use one universal exposure indicator

allowing for a standard mean content of fumes. The evaluation of exposure should be based on the results of measurements of particular elements of fumes in the welders' breathing zone.

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